

SERVICE MANUAL

F 1030

FREQUENCY DIVIDING NETWORK



SINCE 1887



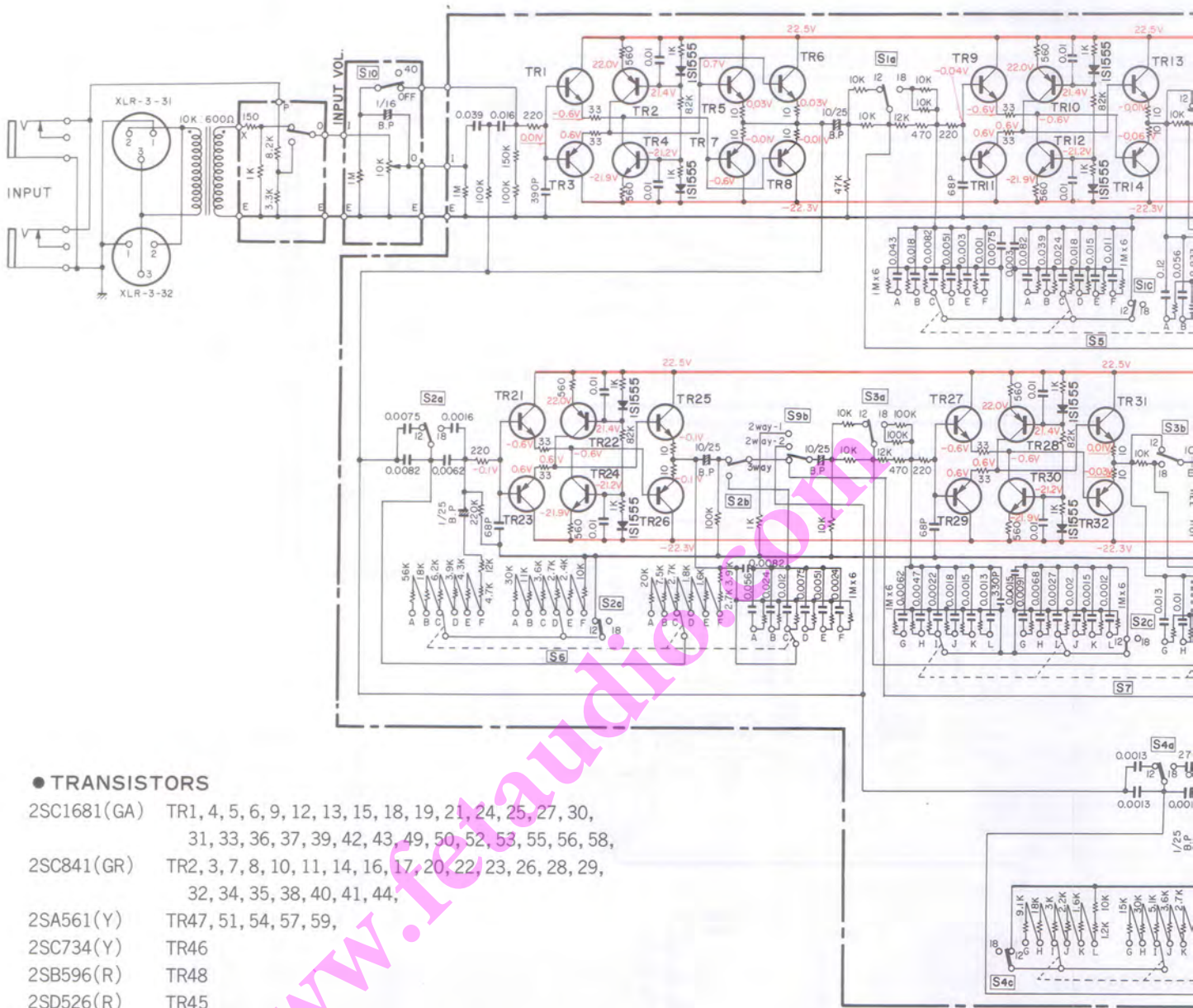
YAMAHA

NIPPON GAKKI CO., LTD. HAMAMATSU, JAPAN



1500 Printed in Japan

SCHEMATIC CIRCUIT DIAGRAM



● **TRANSISTORS**

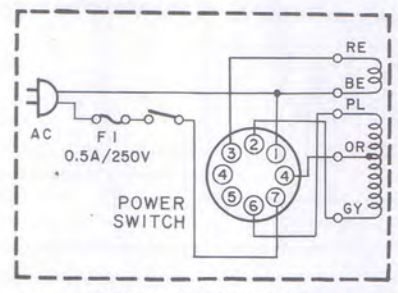
- 2SC1681(GA) TR1, 4, 5, 6, 9, 12, 13, 15, 18, 19, 21, 24, 25, 27, 30,
31, 33, 36, 37, 39, 42, 43, 49, 50, 52, 53, 55, 56, 58,
- 2SC841(GR) TR2, 3, 7, 8, 10, 11, 14, 16, 17, 20, 22, 23, 26, 28, 29,
32, 34, 35, 38, 40, 41, 44,
- 2SA561(Y) TR47, 51, 54, 57, 59,
- 2SC734(Y) TR46
- 2SB596(R) TR48
- 2SD526(R) TR45

● **SWITCHES**

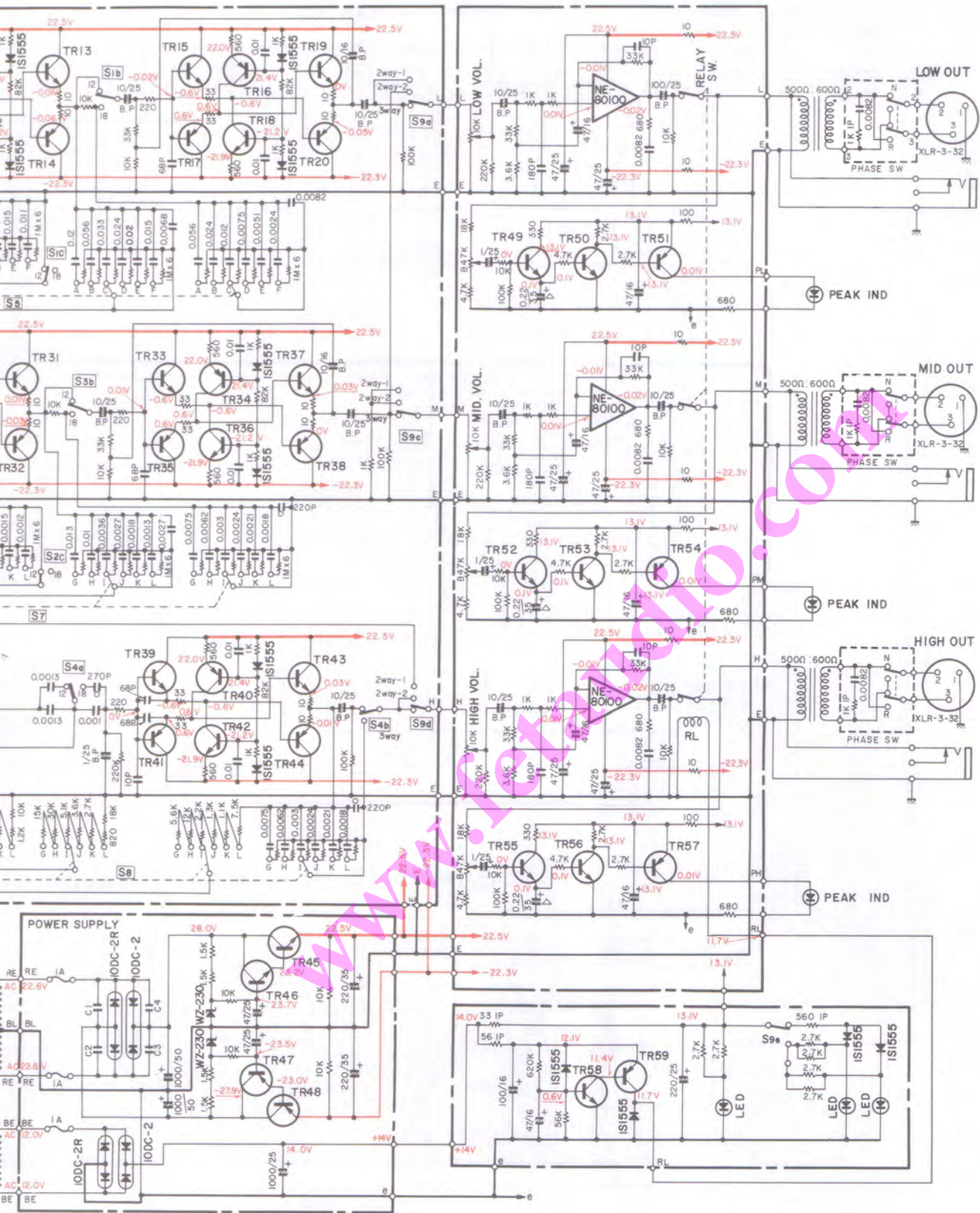
- S1~S4 FREQUENCY RESPONSE SELECTOR (-12dB/OCT, -18dB/OCT)
- S5~S8 CROSSOVER FREQUENCY SELECTOR
A 250Hz B 500Hz C 800Hz D 1KHz E 1.2KHz F 1.5KHz
G 2KHz H 2.5KHz I 5KHz J 6KHz K 7KHz L 8KHz
- S9 MODE SELECTOR
- S10 40Hz HIGH PASS FILTER

● **CAPACITORS**

- C1~C4 0.0047μF/500V(CERAMIC)
- △ TANTALUM CAPACITOR
- STYROL CAPACITOR
- NO MARK MYLOR or CERAMIC CAPACITOR

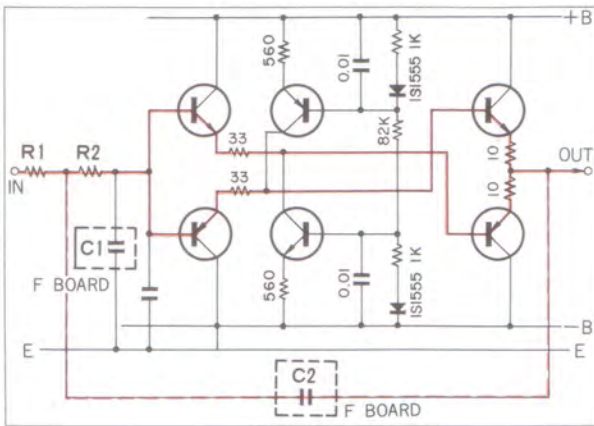


GENERAL EXPORT MODEL



OUTLINE OF CIRCUITS

CR elements, and also -6dB/oct. attenuation characteristics obtained by means of NF.



Cutoff frequency f_c can be calculated by the following equation:

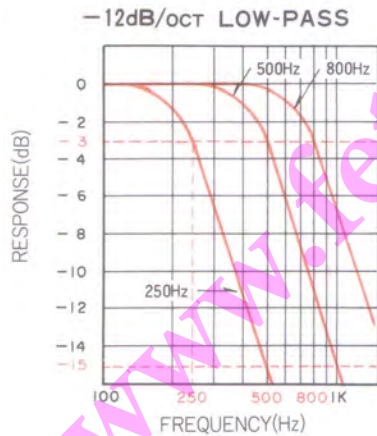
$$f_c = \frac{1}{2\pi \cdot C1 \cdot R2} = \frac{1}{2\pi \cdot C2 \cdot R1}$$

where,

C1, C2: Farad (F)

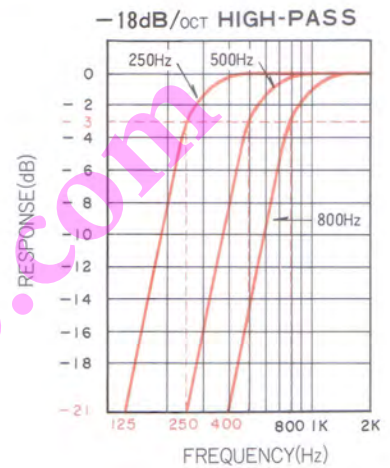
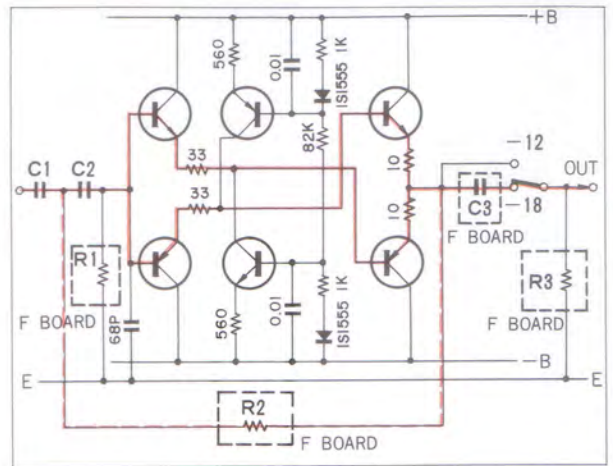
R, R2: Ohm (Ω)

C1 and C2 are combined capacity value in F board (filter element board).



-18dB/oct.

Both high-pass and low-pass filters obtain a characteristic of -18dB/oct. by connecting one stage of CR filter to the output section of the buffer. The high-pass filter of HIGH channel is directly connected to the line amp without using butter at the next stage. As a result, another stage of CR filter is composed of the capacitor at F board and the input volume ($10\text{k}\Omega$) at the line amp.



Gain at Crossover Frequency Points

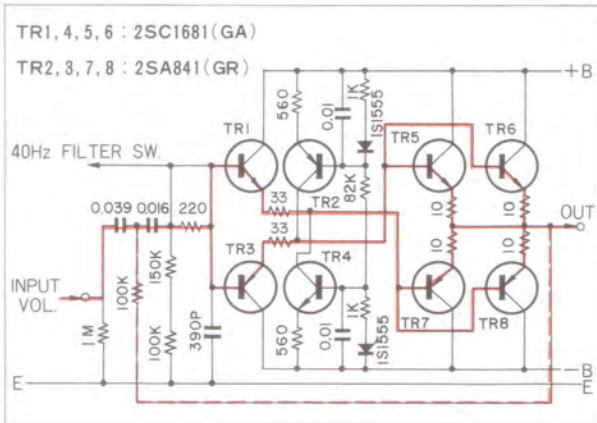
At -12dB/oct. , gain at crossover point (cutoff point) is -3dB at both low-pass and high-pass. This value shows voltage ratio when $\zeta = \sqrt{2}/2$. When converted into output ratio (power ratio), this value becomes $1/2$. Accordingly, the total value of both high-pass and low-pass at crossover point becomes 1. Then, when $\zeta = 1$, the total voltage becomes 1, and the total output (power) becomes 0.5. The difference between the total voltage and total output appears as auditory difference. (ζ : attenuation coefficient)

In case of -18dB/oct. , both the total voltage and total output become 1 respectively.

OUTLINE OF CIRCUITS

The circuits comprise a buffer amp circuit for active filter, three line amp circuits, three peak indicator amp circuits, relay-driving circuit and power supply circuit.

Input Buffer Amp



TR1 and TR3 respectively constitute emitter followers for TR2 and TR4 which are constant-current circuits servicing as emitter resistances. TR1 and TR3 also function as buffer amps having high input impedance. TR5, TR6, TR7 and TR8 are parallel push-pull SEPP circuits which feature great dynamic range and low output impedance. The SEPP circuits are driven by TR1 and TR3. The above-mentioned circuit system is similar to that employed in other filter amps. More specifically, the input amp further reduces output impedance, thus supplying enough power to three LOW, MID and HIGH systems.

In these high impedance input and low impedance output amp systems, CR value is easily established because CR effect on time-constant element is minimized.

In other words, when affected by input and output impedance, CR value becomes complicated and cannot be easily established by calculation.

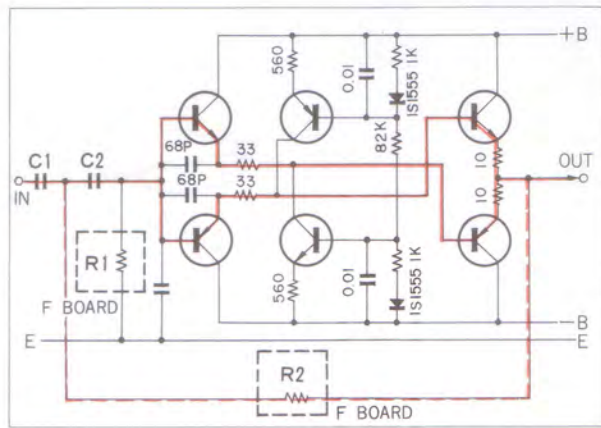
High-Pass Filter

HIGH channel and MID channel each are provided with one high-pass filter circuit.

The high-pass filter consists of the SEPP buffer and feeds low impedance signal with less distortion to the next stage.

Actuation of each transistor in the buffer is basically similar to that of the input buffer. Like other buffer filters, there are two functions – parallel operation and single operation of the SEPP.

Hereinafter, circuit operation at -12dB/oct. will be described.



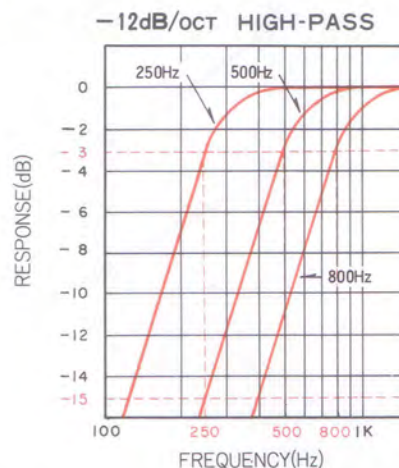
When the signal enters the buffer, low cutting of the signal is conducted at -6dB/oct. by means of C2 and R1. Cutoff frequency (f_c) can be computed as follows:

$$f_c = \frac{1}{2\pi \cdot C_2 \cdot R_1} \quad \text{where, } C_2: \text{ Farad (F)} \\ R_1: \text{ Ohm } (\Omega)$$

C2 includes floating capacity. R1 is combined resistance value in F board (filter element board). Signals emitted from the buffer are fed back through R2. At this time, the signals are attenuated at -6dB/oct. by means of R2 and C1. Now, cutoff frequency f_c is:

$$f_c = \frac{1}{2\pi \cdot C_1 \cdot R_2} \quad \text{where, } C_1: \text{ Farad (F)} \\ R_2: \text{ Ohm } (\Omega)$$

As described above, filter characteristics of -12dB/oct. is achieved from -6dB/oct. attenuation by means of CR passive elements and from -6dB/oct. attenuation by means of NF.



Low-Pass Filter

At the input section of the buffer, -6dB/oct. attenuation characteristics can be obtained by means of